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ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-13) LAUNCH

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Systems Dynamics Laboratory

May 1984



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TECHNICAL MEMORANDUM

ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-13) LAUNCH

I. INTRODUCTION

This report presents an evaluation of the atmospheric environmental data taken during the launch of the Space Shuttle/STS-13 vehicle. This Space Shuttle vehicle was launched from Pad 39A at Kennedy Space Center (KSC), Florida, on a bearing of 91 deg east of north at 1358 UT (0858 EST) on April 6, 1984.

This report presents a summary of the atmospheric environment at launch time (L+0) of the STS-13, together with the sequence of prelaunch Jimsphere measured winds aloft profiles from L-14 hr through liftoff. The general weather situation for the launch and flight area is described, and surface and upper level wind/thermodynamic observations near launch time are given. Since the ship Redstone was unavailable for STS-13 duty, the SRB descent/impact atmospheric data were not taken. However, one can use the STS-13 ascent data for SRB studies, as the best substitute.

Previous MSFC-related launch vehicle atmospheric environmental conditions have been published as Appendix A of individual MSFC Saturn Flight Evaluation Working Group reports [1]. Office memorandums have been issued for previous flights giving launch pad wind information. A report has also been published [2] which summarizes most launch atmospheric conditions observed for the past 155 MSFC/ABMA-related vehicle launches through SA-208 (Skylab 4). Reports summarizing ASTP, STS-1 through STS-11 launch conditions are presented in References 3 through 13, respectively.

II. SOURCES OF DATA

Atmospheric observational data used in this report were taken from synoptic maps made by the National Weather Service, plus all available surface observations and measurements from around the launch area. Upper air observations were taken from balloon-released instruments sent aloft from Cape Canaveral Air Force Station (CCAFS). High-altitude winds and thermodynamic data were measured by the Super-Loki rocketsondes launched from the CCAFS. Table 1 presents a listing of systems used to obtain the upper level wind profiles used in compiling the final ascent meteorological data tape. Data cutoff altitudes are also given in Table 1.

III. GENERAL SYNOPTIC SITUATION AT LAUNCH TIME

An area of weak high pressure, centered just south of Louisiana, prevailed over the southeast just prior to STS-13 liftoff. This new air mass brought cooler and dryer conditions to the KSC area throughout the countdown period. Moderate, west to northwesterly surface winds were the rule during the countdown period. Figure 1 presents the surface map conditions approximately 2 hours before STS-13 launch. Figure 2 depicts winds aloft conditions at the 500 mb pressure level approximately 2 hours before launch. Westerly winds dominated the flow aloft over the KSC Florida area.

Skies were mostly clear throughout the morning of April 6, 1984. Figure 3 presents the GOES-5 visible picture taken at 1400 UT (2 minutes after liftoff). Figure 4 shows an up-close visible shot of the Florida peninsula as recorded by GOES-5, taken at 1400 UT.

IV. SURFACE OBSERVATIONS AT LAUNCH TIME

Surface observations at launch time for selected KSC locations are given in Table 2. Included are pad 39A, shuttle runway, and CCAFS balloon release station observations. Neither precipitation nor lightning was observed at launch time.

Table 3 presents Pad 39A wind data along with other standard hourly meteorological measurements and sky observations for the 6-hr period prior to launch of STS-13. Values for wind speed and direction are given for the 84 m (275 ft) FSS reference level and 18 m (60 ft) pad light pole level.

V. UPPER AIR MEASUREMENTS DURING LAUNCH

The FPS-16 Jimsphere (1413 UT), MSS Rawinsonde (1401 UT), and Super-Loki Robin (1658 UT) systems were used to measure the upper level wind and thermodynamic parameters for STS-13 launch. At altitudes above the rocket-measured data, the Global Reference Atmosphere (GRA) [14] parameters for April KSC conditions were used. A tabulation of the STS-13 final meteorological data for ascent is presented in Table 4 which lists the wind and thermodynamic parameters versus altitude. A brief summary of parameters is given in the following paragraphs.

A. Wind Speed

At launch time, wind speeds were 21.5 ft/sec (11.3 km) at 60 ft and increased to a maximum of 176 ft/sec (104 km) flowing from 289 deg. This maximum occurred at an altitude of 37,700 ft (11,491 m). The winds decreased above this level as shown in Figure 5. The overall maximum measured speed was at 37,700 ft (11,491 m) altitude.

B. Wind Direction

At launch time, the 60-ft wind direction was from the northwest (320 deg) and shifted into a westerly component above 12,600 ft (3840 m). Winds remained westerly through 67,000 ft (20,422 m) altitude. Winds above this level shifted into an easterly component, but came back to be a westerly wind above 123,000 ft (37,490 m). Wind directions oscillated enormously above 180,000 ft (54,864 m). Figure 5 shows the complete wind direction versus altitude profile. As shown in Figure 5, wind direction became quite variable at altitudes with low wind speeds.

C. Prelaunch/Launch Wind Profiles

Prelaunch/launch wind profiles presented in Figures 6 through 9 were measured by the Jimsphere FPS-16 system. Data are shown for four measurement periods beginning at L-13 hr and extending through L+0.

The wind speed and direction profiles for the 13-hr period prior to and including L+0 are shown in Figures 6 and 7. The in-plane (head-tail wind) and out-of-plane (left-right crosswind) profiles are given on Figures 8 and 9. The wind speeds and component speeds were greater than the April means but less than the 95 percent values within the 30,000 ft to 50,000 ft altitude layer, however, no ascent load exceedences were calculated. Unusually strong wind speeds exceeding the 99 percent values measured at L-27 hr and L-50 hr below 20,000 ft altitude produced some calculated load exceedences and some concern early in the prelaunch period. These particular wind speeds subsided as predicted and were not a problem after L-24 hr.

D. Thermodynamic Data

The thermodynamic data taken at STS-13 launch time, consisting of atmospheric temperature, dew-point temperature, pressure, and density have been compiled as the STS-13 ascent meteorological data and are presented in Table 4. The vertical structure of temperature for the STS-13 ascent is shown graphically versus altitude in Figure 10.

The atmospheric thermodynamic parameters of temperature, pressure, and density, measured during STS-13 launch below 163,000 ft (49,682 m) were all within 7 percent of their respective PRA-63 [15] annual values. All these parameters stayed within 13 percent of their respective PRA-63 values, at all levels of measurement.

E. SRB Upper Air and Surface Measurements

As has been mentioned in the introduction, since there was no ship available, an SRB descent meteorological data tape has not been constructed. The tabular values for the ascent meteorological tape as presented in Table 4 should be used for SRB descent/impact studies since it is the closest measured data source.

VI. ATMOSPHERIC SUMMARY CONDITIONS FOR STS LAUNCHES

Given in Table 5 are selected atmospheric L+0 launch conditions for all the Space Shuttle launches.

TABLE 1. SYSTEMS USED TO MEASURE UPPER AIR WIND DATA FOR STS-13 ASCENT

TABLE 2. SURFACE OBSERVATIONS AT STS-13 LAUNCH TIME

							Sk	Sky Cover		Wind	
. Location a	Time After L+0 (min)	Pressure (MSL) N/cm ² (psia)	Temperature ^o K (°F)	Dew Point °K (°F)	Relative Humidity (%)	Visibility km (miles)	Cloud	Cloud	Height of Base Meters (ft)	Speed ft/sec (kt)	Direction (deg)
NASA Space Shuttle Runway X68 ^e Winds Measured at 10.4 m (34 ft)	0	10.156 (14.730)	288.9 (60.3)	279.8 (44.0)	55	16 (10)	0	Clear	1	16.9 (10.0)	310
CCAFS XMR ^C Surface Measurements	+	10.156 (14.730)	289.8 (62.0)	280.4 (45.0)	54	16 (10)	0	Clear	:l	13.5 (8.0)	310
Pad 39A ^d Lightpole NW 18.3 m (60.0 ft)	0	10.156* (14.730*)	288.9 (60.4)	280.2 (44.7)	56	t	ı	I	ı	21.5 ^b (12.7)	320 _p
Pad 39A FSS (Top NW) 83.8 m (275 ft)	0	ŧ	1	; ;	J .	1	.I	1	ı	18.6 ^b (11.0)	275 ^b

*Pad 29A Camera Site 3 barometric pressure instrument appeared to be reading too high. Therefore, the KSC Shuttle runway station pressure value interpolated to 10.149 N/cm^2 at 21 ft above MSL was used as the L+0 pad atmospheric pressure measurement.

a. Altitudes of measurements are above natural grade, except where noted.

b. Approximately 1 min average prior to L+0.

c. Balloon release site.

Pad 39A thermodynamic measurements are taken at camera site No. 3, approximately 6.4 m (21 ft) above MSL. d.

e. Official STS-13 sky observational site.

STS-13 PRE-LAUNCH THROUGH LAUNCH KSC PAD 39A METEOROLOGICAL MEASUREMENTS^a TABLE 3.

					 					
	ć	Otner Remarks								
q _u		vis. (mi)	10	10	10	10	&	8	6	10
Sky Condition ^b	Total	Sky Cover	0/10	1/10	0/10	0/10	1/10	0/10	0/10	0/10
Sky		Clouds	Clear Skys	Scattered at 3000 ft	Clear Skys	Clear Skys	Scattered at 4000 ft	Clear Skys	Clear Skys	Clear Skys
	veľ)	WD°	299	301	284	281	277	283	301	320
	60' Level (NW)	WS Kt	6	10	∞	2	∞	œ	ŢŢ	13
	evel)	мΩо	253	258	253	249	229	231	255	275
rements	275' Level (NW)	WS Kt	12	13	10	10	П	11	6	11
Measu	110	жн (%)	79	82	84	80	82	82	99	56
spheric	Dew	(°F)	47	47	47	45	47	46	44	45
Hourly Atmospheric Measurements	S S E	(°F)	53	53	51	51	52	52	56	09
Hour	100 t times A	o April 1984	0400	0080	0060	1000	1100	1200	1300	L+0 ^c 1358

Hourly pad observations (obtained via MSFC/HOSC) averaged over 2 min, centered on the hour.

b. Sky observations taken at the Shuttle runway site X68.

L+0 PAD Wind and thermodynamic parameters obtained from HOSC strip charts. NW Anemometers used at 60 and 275 ft levels for L+0 wind conditions (approximately 1 min average prior to L+0). Pad 39A L+0 atmospheric pressure, at 21 ft (MSL), was 10.149 N/cm². Sea level pressure was 10.156 N/cm^2 . ပ

TABLE 4. STS-13 METEOROLOGICAL DATA TAPE ASCENT

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0.00 0.34 3.07 8.8 .9210+03 0.00 0.35 3.13 8.8 .9176+03 0.00 0.35 3.13 8.3 .9176+03 0.00 0.35 3.10 7.8 .91042+03 0.00 0.35 3.10 7.8 .9075+03 0.00 0.35 3.10 7.3 .9008+03 0.00 0.30 3.14 6.4 .8975+03 0.00 0.28 3.14 6.4 .8975+03 0.00 0.28 3.14 6.4 .8975+03 0.00 0.28 3.14 6.4 .8975+03 0.00 0.28 3.14 6.4 .8843+03 0.00 0.28 3.10 6.3 .8843+03 0.00 0.31 3.10 5.4 .8745+03 0.00 0.34 3.05 5.4 .8748+03 0.00 0.34 3.05 5.4 .8748+03 0.00 0.34 <t< td=""><td>260 03 200 03 200 03 200 03 200 03 200 03 200 03 200 03 200 03 200 03</td><td></td><td>1 C</td><td>9 € • 0</td><td>0.44.40</td><td>11128+D4</td><td>, ,-</td></t<>	260 03 200 03 200 03 200 03 200 03 200 03 200 03 200 03 200 03 200 03		1 C	9 € • 0	0.44.40	11128+D4	, , -
0.00 0.35 3.05 9.05 9.176+03 0.00 0.35 3.12 8.6 9.142+03 0.00 0.32 3.10 7.8 9.109+03 0.00 0.35 3.05 7.6 9.075+03 0.00 0.33 3.15 7.4 9.048+03 0.00 0.33 3.15 7.3 9.075+03 0.00 0.27 3.14 6.8 8942+03 0.00 0.27 3.14 6.8 8942+03 0.00 0.28 3.09 6.6 8942+03 0.00 0.28 3.10 6.6 8942+03 0.00 0.31 3.10 6.1 8843+03 0.00 0.32 3.10 6.1 8811+03 0.00 0.34 3.0 5.6 8778+03 0.00 0.34 3.0 5.6 8778+03 0.00 0.34 3.0 5.4 8616+03 0.00 0.34 3.0	200 033 05 05 05 05 05 05 05 05 05 05 05 05 05			d 0	9210+0	-1135+04	-
90 90<	200 03 200 03 200 03 200 03 200 03 200 03 200 03 200 03 200 03		3,13) v	0176+0	1131404	
000 035 310 8.1 9/109+03 000 035 305 7.6 9/109+03 000 033 310 7.5 9/109+03 000 033 310 7.5 9/109+03 000 030 314 6.8 8/972+03 010 027 314 6.8 8/972+03 010 027 314 6.8 8/972+03 020 031 310 6.8 8/972+03 021 310 6.3 8/843+03 022 310 6.3 8/843+03 030 310 5.4 8/843+03 031 310 5.6 8/75+03 031 310 5.6 8/75+03 031 312 5.6 8/75+03 032 312 5.4 8/81+03 031 312 5.3 8/648+03 031 312 5.3 8/814+03 032 31	200 03 20		717	ο α	0142+0	,1128+04	-7
100 0.35 3.05 7.6 9075+03 100 0.35 3.06 7.1 9042+03 100 0.30 3.10 7.1 9008+03 100 0.30 3.14 6.8 9942+03 100 0.27 3.14 6.8 8975+03 100 0.21 3.09 6.6 8975+03 100 0.31 3.0 6.3 8843+03 100 0.32 3.0 8811+03 100 0.34 3.0 8778+03 100 0.34 3.0 8748+03 2.0 0.34 3.0 8648+03 2.0 0.34 3.0 8.6 2.0 0.34 3.0 8.4 2.0 0.34 3.0 8.4 2.0 0.34 3.0 8.4 2.0 0.34 3.0 8.4 2.0 0.34 3.0 8.4 2.0 3.0 8.4	200 03 400 03 500 03 500 03 500 03 500 03		- C) ⊷ • • • •	0+6016	.1125+34	
200 7.6 9042+03 500 033 310 7.3 908+03 500 030 315 7.1 8975+03 500 030 314 6.8 89042+03 500 027 314 6.8 8909+03 500 021 304 6.3 88442+03 500 031 310 6.3 88442+03 500 031 310 6.3 8843+03 500 032 310 6.3 8843+03 500 034 30 8714+03 500 034 30 8713+03 500 034 30 8713+03 500 034 30 8648+03 500 034 30 8648+03 500 034 30 8648+03 500 034 30 80 80 501 502 80 80 80 601 602	200 500 500 500 500 500 600 600 600 600 6		3.05	7.8	9075+0	.1122+D4	
500 033 310 7.3 .9908+03 100 030 314 6.8 .8975+03 500 027 314 6.8 .8904-03 500 021 30 .6.3 .8876+03 500 031 310 6.3 .8876+03 500 030 310 6.3 .8843+03 500 034 30 8811+03 500 034 30 8778+03 500 034 30 8713+03 500 034 30 861+03 500 034 30 861+03 500 034 30 8648+03 500 034 30 8648+03 500 034 30 8648+03 500 034 30 8648+03 500 034 30 8648+03 600 034 30 8648+03 600 034 30 8648+03	500 500 500 500 500 500 600 600 600 600		306	7.6	9042+0	•1119+Ud	
100 031 315 7.1 .8975+03 500 027 314 6.8 .89042+03 500 021 309 .8909+03 500 031 306 6.3 .8876+03 500 030 310 8811+03 500 038 304 5.6 .8778+03 500 039 304 5.6 .8778+03 500 034 309 5.4 .861+03 500 034 309 5.4 .861+03 500 034 309 5.4 .861+03 500 034 309 5.4 .861+03 500 034 309 5.4 .861+03 500 034 30 5.3 .8584+03 500 034 30 5.3 .8584+03 500 034 30 5.3 .8552+03 500 034 30 5.3 .8552+03 500	500 02 500 02 500 02 700 03		310	7.3	9008+0	#D+9###	
5GD 027 314 6.8 .8942*U3 5GD 028 359 .66 .8909*U3 5GD 031 326 6.3 .8843*C6 .8843*C6 7GD 030 310 6.1 .8843*C6 .8778*C6	500 02 500 02 700 03		315	7.1	8975+0	#0+0 TTT*	
5ug UZB 5ug 6.3 8876+03 7ug 031 3ug 8814+03 7ug 031 3ug 8814+03 9ug 036 3ug 8814+03 9ug 3ug 8011+03 9ug 3ug 8778+03 10ug 038 3ug 8713+03 10ug 034 3ug 8713+03 10ug 034 3ug 8713+03 10ug 034 3ug 848+03 10ug 034 3ug 848+03 10ug 033 3ug 848+03 10ug 034 3ug 8ug 10ug 034 3ug 8ug 10ug 034 3ug 8ug 10ug 033 3ug 8ug 10ug 034 3ug 8ug 10ug 034 3ug 8ug 10ug 034 3ug 8ug 10ug 034 <td>700 03 700 03</td> <td></td> <td>314</td> <td>20 V</td> <td>394240</td> <td>######################################</td> <td></td>	700 03 700 03		314	20 V	394240	######################################	
7uc 6.1 8843+63 11 9cc 031 310 6.1 8811+03 11 9cc 036 36 8811+03 10 10 036 36 8778+03 10 100 039 364 8713+03 10 200 039 309 5.5 8713+03 10 400 034 309 5.4 868+03 10 400 033 306 5.4 8648+03 10 50 034 306 5.4 8648+03 10 50 5.3 8648+03 10 50 5.3 8648+03 10 50 5.3 8648+03 10 50 5.3 8648+03 10 50 5.3 8648+03 10 50 5.3 8648+03 10 50 5.3 8648+03 10 50 5.3 8648+03	0.00		3.07	200	P R 76+C	1103+04	•
900 5.8 .8811+03 .10 900 5.6 .8778+03 .10 900 35 35 .8778+03 .10 900 35 35 .8713+03 .10 100 639 35 .8713+03 .10 300 33 308 5.4 .8681+03 .10 500 634 304 .8648+03 .10 500 634 304 .8648+03 .10 500 634 307 .8648+03 .10 500 634 307 .8644+03 .10 501 634 307 .8644+03 .10 502 303 .312 .323 .8644+03 .10	つここ		0 5	o 40	8843+0	1100+04	•
0.0 0.36 3.6 8.778+03 10 100 0.38 3.64 5.6 .8713+03 .10 100 0.39 3.05 5.4 .8713+03 .10 300 0.34 3.09 5.4 .8681+03 .10 4.0 0.33 3.06 5.4 .8648+03 .10 5.0 0.34 3.06 5.3 .8648+03 .10 5.0 0.34 3.06 5.3 .8648+03 .10 5.0 0.34 3.07 5.3 .8554+03 .10 7.0 0.32 3.12 5.3 .8554+03 .10	7.7	and the second s	212	000	8811+0	• 109 7+04	•
100 638 364 5.6 • 8745+03 • 109 100 639 305 5.5 8713+03 • 108 200 634 309 5.4 861.63 • 108 300 633 306 5.3 8648+03 • 107 500 634 306 5.3 8616+03 • 107 500 632 312 5.3 8524+03 • 106 700 632 312 5.3 8532+03 106			3.0) vo	8778+0	1394+	•
5.5 .8713+03 .108 309 309 5.4 .8681+03 .108 300 034 309 5.4 .8648+03 .108 400 033 306 5.3 .8648+03 .107 500 034 307 5.3 .8584+03 .106 501 307 5.3 .8584+03 .106 502 312 5.3 .8552+03 .106			₹74		0+5+1	2	7
309 5.4 . 4681+C3 . 108 300 033 308 5.4 . 8648+03 . 107 500 033 306 5.3 . 8616+03 . 107 500 034 307 5.3 . 8584+03 . 106 700 32 312 5.3 . 8584+03 . 106 700 5.3 . 8552+63 . 106 . 106					8713+0	108	7
450 033 308 5.4 .9648*03 .1079 450 C35 306 5.3 .8616*03 .1075 550 C34 307 5.3 .8584*03 .1068 700 312 5.3 .8552*03 .1068 700 312 5.3 .8552*03 .1068			60.5		681+C	1083+	-2
500 C35 326 5.3 .8616+03 .1075 500 G34 , 327 5.3 .8584+63 .1072 700 G32 312 5.3 .8552+03 .1068 700 G32 312 5.3 .8552+03 .1068) M		308		0+8+9	1079+0	(1)
5.0 634) 327 5.3 .8584+63 .1972 707 632 312 5.3 .8552+63 .1068	50.0		306		616+0	1075+0	-2-
700 032 312 5.3 .9552+03 .1068	500	-	307		584+0	1072+0	5
100 C C C C C C C C C C C C C C C C C C	700	The state of the s	312		552+0	068+0	7) (
300 035 308 300 035	038		308		52	100	•

ETEOROLOGICAL DAT	A TAPE	(L	PRESSURE	NSIT	POI
Ħ	ND SPE		(1) 5 (1)	ا	GRAMI	ر
F	1/SE	(DEG)	1	2+157+6	157+0	•
335030	M :	\$12	4 M	426+0	352+	•
005100	m	9 (1 M 1	ា ជា • (ក ជ	395+0	1048+	-
005500	₩.	248	α · · · · · · · · · · · · · · · · · · ·	364+0	1043+0	•
JUS 300	m	2 P	, v	333+0	036+0	6
.05400	M:	710	6.2	8302+0	1034+0	3.0
005500	m I	30.00	1 3 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	8271+0	1030+0	2.21-
005600	M	100	9.9	8240+0	1025+	•
0.057.00	045	⊒ • 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.9	.8210+03	20+0	
.05800	31	400	7.1	8180+0	*1016+04	
205900	3	n 0	M. C.	0+6718	112+0	
006000	# # O	667	7.7	8119+0	0.8+0.0	
006100	50 at 50	867) h	A 089+0	0 + + 0	_1
.0620C	04.2	3 i.1	7.0	8059+0	101+0	17.
006300	9 00	30.5	7.7	Ü	69	-
006430	640	101	7.7	9000+0	33+5	-17.0
006500	CSO	3 th	4 C	7970+0	397+0	- 1
009900	ከቱር	307	701	7941+0	361+	•
006700	770	M	7.1	9 0	325+0	-1
506300	045	298	T • /	7887+0	190+0	
0690p	540	301) C	154+0	- 4
000267	042	303	101	7874+	720+0	-
1,07100	042	298	→ (C	7 7 0 7 4 7	585+0	- 4
U07200	740	295	0.1	7766+0	551+0	
007300	740	262) • •	3.U	16+	-170
007400	045	297	7.00	7+6047	9582+	-17.2
007500	940	293	0 4 0 4	+	48456	-17.
00920	048	162	6.0 0	7657+	9514+	-17.
0770	5 4 0	262	ο ·	, <u> </u>	+3846	-17.
00870	8 7 0	290	8.0	7505+	+9446	-17.
007960	051	289	· • • • • • • • • • • • • • • • • • • •	+	9413+	-17.
00800	D54	291	1.0	7530	9378+	-17.
001800	055	294	· 1 · · · · · · · · · · · · · · · · · ·	45474	9344+	-17.
08200	C 5 3	294	100	7484+	310+0	-17
008300	057	D 66	- P	+	-	-17.6
008400	090	29.0	4 4	7428+	242+0	.7.
0.085.00	0.55	767	, d	7401+	208+0	-1/-
008600	056	5.42	4.4	7373+	9174+0	.17.
JO8 70C	& (C)	2 6 2 6	9	7346+	-	- 1
008800	650	262	9.9	7319+	0.4 0.4 0.4 0.7	1 1
208807	7.00) (C	- 9	+	73+0	0 1
00000	000	201	† 9	+	10 + S1 +	9 4
00,100	/ n i	0 0 0 0	т. 9	+	7	011
2	C 2 9	FOR	6.1	+	988+1	**************************************
M	100	0 × 0 ¢) v	+	960+0	7 0 1
3	0 0 0	205	8.5	+	932+0	0 .a
N)	۵ ا ۱ م ا	0.00	. 10 10 10 10 10 10 10 10 10 10 10 10 10 1	+	++06	0
009600	753	100	5.5	105		* 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
_	0.0	, o	ស	+	8484	
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TABLE 4. (Continued)

TUDE	SPE	1	ERAT	FSSURE	ENSIT	0
FT)	(FT/SEC)	(056)	(DEG C)	ILLIBAR	RAMIM	DEG
1000	S	ωį	5.0	056+0	793+0	œ
1010	2	œ.	80. * :#	0+6669	8766+0	6
1020	9	α):	9.4	973+0	740+0	6
1030	9	ω.	ਕ : ਕ :	947+0	7.14+3	13
1040	Ð,	ത്ര	4 • 2	6921+0	8687+7	5
2 :	<u> </u>	1000	ים מילי	5895+040 1040+040	*8661+US	* 0 * 1 * 1
1060	ا (0	0 1	0.0	0 1 0 1 0 1		
20,000	so ,	သာပ			20144	0
on c	οv	ο α	3-2	0 + 2 0 2 4 0	8557+0	12
2 6	0.4	oα	7 C Y	5-69-F	532+0	202
3 C	o' 🗸) (X	7.8	K 747+0	8507+7	20
10) C) (C) in	717+0	482+3	20
	S S	00	2.3	6691+0	8457+3	20
) () uc	2 1 2	666+0	8432+0	20
	Š) (10	6 1	6641+0	8408+0	21
9 (9	9 40	സ	1 6	6616+0	8383+3	21
	9	ι, α	5 • T	6591+0	8358+0	21
8	· 40	100	1.52	566+0	8334+3	21
18	9	w	6.	6542+G	8310+0	23
5	9	ထ	L •	517+0	285+1	21
10	•	ശ	ທຸ	6492+0	8262+3	N
2	9	·ω;	.2	6468+0	238+0	22
30	3	œ	a•	443+0	8214+0	N I
9	0	∞	3	6419+0	190+0	22
ED.	9	တေ	រក ៖ 1	394+0	8167+0	7 1
0	9	m		0 2 / 0 + 0	8 4 3 + 1	
5	so .	നാ	Q.	346+0	0+071	3 5
2	٠ ا ٥	ω) :		22776	0 - 4 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6	3 6
012900	Ø 4	1 œ	ທຸ ເ • • • • • • • • • • • • • • • • • • •	04240		7 6
밁	ola	- 10	-4¦ €	6 4 7 4 0 A C A	A 7 7 + D	7
2 0	O C	- ac	10	226+0	8003+0	5
2	10	1	ķΝ	6202+0	0+086	24
7	•	~	1	178+C	7957+0	24
50	S.	~	M	154+0	7934+0	7 7
င္သ	امت	Ω.	m	6131+0	7911+0	NI
2	so .	-	m,	107+0	7888+0	U L
8 8	٠! ٥	- 1	M :	0+4809	7865+0	U C
) (ο.	~ r	ナ :	04740	7 1 7 1 0	7 0
3 5	יו ס	- 11	3 5	010000	01406	3/4
1410	oσ	- 1	n α • τ τ τ Ι Ι	9 6	777+3	-26.
1 2) 4	- [a	ľ	104040	7740+0	12
	0.4	0 1	າ ແ	0.70	4 4 6	iN
	٠,٠) ; 14	E 0 2	775 340	1
	oν	- 1	7 h	100	ם כ	-27
1470) o) in	876	7656+9	27
142		· r	,		1	1
		÷	,	4	0 + 2 + 3	-

ROLOGICAL DAT	.v.	Đ.	E R	RESSUR	INSTIT	01
00 T 1 3 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	CFT /SFC	(930)	(DEG C)	IBAR	SAM/4	DEG
		, #	9	5808+0	588+0	nil
) u	3) 40	274	9	785+0	565+0	•
01010	٠.	27.1	7	5763+0	542+3	A.
) u	Y	273	-	740+0	7520+0	Λ.
יי ני) v	276	-	5718+C	0+26+	A.I
00.40); J	277	-	5695+0	7475+0	-28.
i r	`	275	8	573+C	7452+0	C) I
l r	ی اد	277	8	5651+0	7436+3	\sim
15820) v	280	00	5629+0	7408+3	rt si
15900	1	277		507+C	385+3	n,
ı vo	ഹ	280	0	5585+0	7363+3	CII (
u so	9	279	Ġ.	563+0	7342+0	N 1
ഹ	S	277	6	5541+0	320+0	NII I
J16300	0	274		2219+0	7298+3	คว เ
9	S	275		2498+0	7277+3	M 11
	3	276	10.	2476+0	25543	~
166	•	273	0	5455+0	7234+1	m.
167		272	Ċ	5433+0	7213+0	m.
- α	S	275	-	5412+0	7191+0	m!
	אוכ	273	-	5390+0	7170+0	P-7
	o c	27.0	, e	5369+0	7149+0	m
) v	276	-	548+0	7127+3	m
) v	310	12	5326+0	105+3	m
). v	274	2	5305+0	7084+0	m
017400) C	27.8	2	284+0	062+0	m:
017500	1 40	278	12.	5263+D	7041+0	m
, .) v	777	3	242+0	019+3	M.
) v	77.	3	5221+0	0+8669	m
, ,	v v	. C:	M	5201+0	976+3	m i
		276	7	5180+0	6955+0	M)
01800	·vo	278	e t	5159+0	6934+0	m i
	140	278	7	5139+D	6913+0	m 1
	တ	275	7	5118+0	892+0	M) .
8	•	277	7	2098+C	871+1	~ 1
18	vo	277	15	5077+0	851+0	
18	ഴ	275	ŭ.	5057+0	E + D E 8	77 1
18	~	274	5	5036+0	8 10+0	71 II
18	9	276	Š	5016+0	C+6819	Y) [
8	9	276	16	0+966	769+3	T) [
18	-	274	16.	0+9/6#	1 4 8 4 1	กก
19	v	277	16.	4926+0	728+0	*1 f F
019100	190	276	-16.9		6708	1 1
6	SO.	275	17	4916+0	+889	n ; ,
12	o	277	7.	4896+0	668+3	Y) P
3	•	277	17.	4876+0	648+1	
1950	O.	276	17.	856+0	628+3	~ }
960	9	277	8	4837+0	608+0	7)[[
1970	vo	276		817+0	288	٠,
					40.71	r

TABLE 4. (Continued)

WIND DIPE
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23# 238#
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010 010 010
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780
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7 6
2 6
26
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TABLE 4. (Continued)

ALTITUDE	SPE	D.	A.	URE	ENSIT	8
(FT)	(FT/SEC)	(030)	CEG C	ILLIBAR	AMIN	DEG C
0.30 0.00	142	-001	37	112+C	10	N
0	7	ω	-	098+C	583+0	52.
ນ 30 2 ປີຕ	3	ത	~ i	385+0	7+3	25
	146	(0)	ω	071+0	550+0	52.
239460	145	.co	10	056+C	533+0	52.
C 30 500	#	σ	€38.4	0+440	<u>.</u>	25
030600	4	(10)	ω,	031+0	500+0	52.
0.30700	S	ധ	00	117+0	• 4483+03	52.
J3380C	S	ON!	00	004+0	.4467+03	52.
0.30,600	S	æ	O.	991+0	• 4450+03	52
031000	W,	CO)	O.	978+0	• 4424+O3	53.
031100	S	o	O	965+G	• 4417+03	53.
J3120C	w)	ωı	-39.4	951+D	. 4399+03	53,
031300	S	100	-39.6	938+C	.4382+03	53.
J3140C	10	O.	-39.7	925+0	.4365+03	53.
.31500	1	ιo	-39.8	912+D	• 4348+D3	53.
.3160D	· w	ယေ	6.68-	0+006	• 4331+03	53.
u3170C	1	ന	0.04-	387+C	.4314+03	54.
G31800	ഹ	ထ	-4C+2	874+D	. 4297+D3	54.
J31900	l w	lα	-40.3	361+C	.4280+33	540
0.32000	ະທ	σ)	4.04-	348+0	.4263+33	54.
J32100	'n	00	-40.5	336+0	.4246+03	54.
032200	LO.	œ	-40.6	823+D	• 4230+03	540
032300	រហ	00	8.04-	311+0	.4213+03	5.4
J32400	S	83	6.04-	798+C	.4196+03	54.
.325 00	5	œ	-41.0	786+0	.4180+33	54.
C32600	N)	00	T 9 17 17 18	773+0	.4163+73	IO!
0327a 0	S	(I)	-41.2	761+0	• 4147+03	54.
032800	S	(1)	4° [n-	146+0	.4131+03	55.
u32900	S	no	-41.5	736+0	.4114+03	55
.33 000	vo	œ	-41.6	724+0	• 4098+13	55
J33100	9	CO	-41.8	712+0	4083+0	55.
ບ332ພໍດ	O	CO	-42.0	700+0	.4069+03	55
033300	9	ത	-42.2	588+0	• 4054+03	9
033400	~ ∣	യി	-42°4	276+0	.4039+33	2
033500	r 1	ထား	142.6	0.4409	* # O Z S + O Z	n L
U.536U0	- 1	2010	8.77.	1+766	50+010+•	n u
237 / 0.0	- 1	o o				• u
23000	- 1	O X	7001	1440	3067+0	2
	- 1	3 a	T C C C C C C C C C C C C C C C C C C C		0.50+0	9
34100	٠ ۲	s loc	A . 7 11	1034	39 38+7	99
034200	172	000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	581+0	3923+3	9
34 300	-	100	1	0+699	0+636	56.
3 / 3	٠.	oo	- 3	558+0	3894+3	57
10	-	ŧαο		04949	3880+3	57.
~	~	œ	L. 44-	535+0	3866+3	57
U34700	175	285		.2523+03	.3851+33	57.
	174	ത	1454	512+0	837+7	-
١.	l	1	The state of the s			

OGICAL DAT TTUDE	A TAPE WIND SPEED		ER A	RESSURE		IOG M
11100	TI VELL	(010)	(DEG C)	H	(GRAM/M3)	(D)
	174	1 10	-45	2489+0	.3809+03	53.
	174	786	50	78+0	.3795+03.	58
	* * * *	787	0.00	0+99	.3781+03	8
20000	64.	285	9	55+0	.3767+03	မ ယ က
	27.5) 30 30 40	-t6.	0+11	.3753+03	-58.
	140	787	9	33+0	.3739+33	58.
	170	787	യ	22+0	,3726+33	59.
033900	170	287	: 🕠	11+0	.3712+03	29
	0.4	0000	_	2400+5	,3698+03	20
00000	172	788	-	89+0	.3685+33	59.
000480	172	7.60	_	78+0	.3671+03	59.
036100	172	288	٠.	67+0	.3657+03	59
01000	17.2	782	,	56+0	.3644+03	59
36 700	173	287	ω	45+0	.3630+03	50
ייייייייייייייייייייייייייייייייייייי	17.0	0.80	(0)	2334+0	.3617+03	-
2004	174	788	3	24+0	.3603+03	•
200000000000000000000000000000000000000	17.4) (C)		2313+0	.3590+03	-60-
0.000.0	174	288	4	02+0	.3577+03	6
20.00	174	0 00	(,	92+	.3563+03	7-09-
14900	173	288	וט	1113	.3550+03	9
000250	174	287	*49.5	2271+0	.3537+23	٠ إ ن
637100	175	288		2260+0	. 3524+03	ω,
03720	175	288		50+0	.3512+03	. 10
037300	174	287		2239+E	8D+6648.	79.
37400	173	287		2229+	. 3487+03	•19•
037500	174	288		+61	1110000	40
J3760C	175	288		1508+	. 3462+33	• 70 -
037700	176	289		98+	50+00+0 50+00+0	40
037800	176	293		1 8 8 1 7	00 + 00 + 0 •	ıln
037900	175	292		101	40480400	-63
38300	174	289		21574	3401+03	M
0.381.00	174	282		714746	MC+68MM	63
0.582.00	1 7 5	200		37+(.3377+03	M
	0 L	, i c		2127+(.3366+03	- 19-
	175	201		2117+0	.3354+D3	#
000000	7.1	290		2107+0	。3342+J3	or ∫.
78700	174	291		1+1602	.3331+03	# (
000000	174	100		187+	.3319+73	-65
038900	173	290		2078+0	.3308+03	O A
39300	173	291		168+	.3296+03	0
039100	173	262		2058+0	.3283+03	0 u
039200	173	390		2048+	.3270+03	n j v
C3930C	172	290	-55.1	+ 6	3258473	o «c
J 39400	172	290		62	201010	ی ار
039500	171	289		1194	50.524) <u>(</u>
039600	17.1	289		0	227713) (
039700	171	289			* 520 / 105 * 104 pt + 1	Q. C
			•)

TABLE 4. (Continued)

ALLIUDE	2	A TUD DIFFILION	T T T T T T T T T T T T T T T T T T T	TRI VOURE	LENST	
(FT)	(FT/SEC)	_	C	(MILLIBARS)	R A	핃
000	170	288	-56.4	•1972+D3	-	-66.8
010	171	289	9	962	5	0.19-
20	172	290	-56.9	•1953+D3	0	-67.2
300	171	289	~	776	.3135+03	
7	171	289	-57.4	-32	Ç	-67.6
050	171	289	-	925+	p	
0.60	172	289	-58.0	.1916+03	P	-68.1
070	171	289	58	+906	Ç	8
040800	171	290	œ	•	.3079+03	
3	170	290	58	.1888+03	P	-689-
U41000	170	290		.1879+03	-	-68.9
34110C	169	290	5.9	.1870+03	.3043+33	6666-
041200	•	290	-59.2	.1861+03	-	6666-
041300	9	290	O	.1852+03	.3017+03	6666-
041400	168	289	O	843	0++	6666-
341500	•	289	-5.9°5	.1834+03	0+1	6666-
041600	166	288	O	825	-	6666-
041760	9	287	ᠬ	.1816+03		6666-
041800	168	287	C	808+0	•	6666
041900	167	288	6*65-		.2939+03	6666-
.4200E	167	290	-60.D	.1790+⊡3	m,	6666-
042100	•	292	-63.0	.1782+03		6666-
342200	9	292	-60°D	1773	2898+0	6666-
042300	•	293	-63.0	.1764+03	~	6666-
042400	157	293	160.0	***	2870+0	6666-
u42500	n	293	-63.0	.1747+03	2856+0	6666-
04260C	S	294	-60.1	.1739+03	2843+7	6666-
042700	3	294	-60.1	***	2829+0	6666-
042800	4	295	-60.1	.1722+03	~	3
042900	3	294	-60.1	.1714+03	O	6666-
043000	m	294	-60.1	•1705+03		6666-
043100	m	293	-60.2	•1697+D3	•	6666-
U43200	m	293	-60•2	.1689+63	Ci	രി
043300	2	293	•	.1681+C3	Ö.	666
043400	N	290	+°09-	673+0	738+	6666-
043500	N I	290	# (C) (Q) (A)	• 1664+03	2726+0	6666-
043600	N	289	-60.5	656+0	14+1	666
043700	-	782	ro (м,	2701+0	~ 4
043800	2	584		940+0	5	6666-
043900	Ν.	7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	å e	→ •	7 1 97	AAAA
3 .	- 4¦•	207	000	0.4701	10007	100
つ (011 111	0 C	V. 1001	1010101	• K655405	
7	- 1	000	١.	0	0.11.02	
	→	082	16 1.0 U	• 16U1+U3	• 26.74+13 26.17+03	00001
r u	4 -	27.6	****	0.000	0+1070	۱in
70	-1 -	977	•	10801	9 5	6666
0 0	- ا	417	٠.	13/810	7 6	1444-
	4 (612	* = = = = = = = = = = = = = = = = = = =	15/04/03	2534405	66661
	١					

ALTITUDE	D SPE	WIND DIRECTION	ERA	RFSSUR	113	DEW POIN
(FT)	(FT/SEC)	(DEG)	(DEG C)	LLIBAR	(GRAM/M3)	(DEG
0		272	-61	1547+0	•2548+03	• 6666-
4510	132	273	9	539+6	.2536+03	666
20	134	273		532+0	.2524+03	6666-
4530	136	271	-	524+0	.2513+03	6666-
454	134	270	-	517+0	.25C1+D3	6666-
4550	132	269		10+0	.2489+03	6666-
4560	130	267	-62.0	1502+0	.2478+03	6666-
570	131	266	2	495+	.2467+03	6666-
4580	334	267	-62.1	488+	.2455+03	6666-
45	135	268	9	0+084	.2444+03	6666-
600	133	268	-62.2	473+0	.2433+03	6666-
4610	134	267	-62.2	1466+0	.2420+03	6666-
462	133	266	-62.1	1459+0	.2408+03	6666-
630	133	266	-62.1	52+0	.2396+33	6666-
049	135	266	-62.0	1445+0	.2384+03	6666-
4650	137	267	-62.0	1437+0	*2372+33	6666-
4660	- 00 - M1 - H1	268	-62.0	1430+0	*2360+03	6666-
4670	138	270	-61.9	1423+0	*2348+03	6666-
046800	(D)	271	-616	1417+0	.2336+03	6666-
469	139	271	-61.8	1410+0	.2324+03	6666-
	137	27.0	80.19	1403+0	2312+03	66
471	140	268	9	1396+0	*2259+33	6666-
.47200	142	268	9	.1389+03	.2287+33	6666-
473	ይቱፔ	272	-61.4	1382+0	.2274+03	6666-
047400	143	274	-61.03	.1376+03	.2262+03	6666-
047500	146	274	-61.2	369+0	.2249+03	6666-
476	147	276	-61.0	1362+0	.2237+03	6666-
	97	276	0 · 10 ·	155640	\$5.55.00	**************************************
-	14 88	278	86.0	34.740	• ZZ13+U3	*****
06/1	2.52	278	9.1	1342+0	• 2200+03	0.000 0.000
8 0	152	279	-60.5	1336+0	•2188+U3	AAA-
048100	191	278	a	1329+03	.2177+03	6666-
10704	→	117	******	1 2 2 3 + 0	CD 40017 *	****
) (C) (C) (C) (C) (C) (C) (C) (C) (C) (C	917			00 + 00 + 00 + 00 + 00 + 00 + 00 + 00	
) C	001	017	7.04		00.047.	10
	N F = +	017	7.00	1 2041	2122103	h o
0 0	14.6	112	T. CO.	1201+0		000
- α	7 M C		7 O	785+1		000
890	140	281	-59.9	1279+0		66
900	137	280	80 e	1273+0		o
910	133	281	-59.8	266+0		6666-
2.0	127	281	-59.8	260+0	• 2058+03	6
930	122	281	-59.8	1254+0		66
046	119	281	8.65.	1248+0	.2038+03	6666-
4950	116	280	159.8	.1242+03	.2028+03	66
0964	112	280	-59 •8	•1236+D3	• 2018+03	6666-
97	109	279	O	.1230+03	.2008+03	666
4980	107	277	-59.8	.1224+03	•1999+ 03	6666-
0						

TABLE 4. (Continued)

ULUGICAL UATA LTITUDE	WIND SPE	WIND SIRECTION	TEMPERATURE	SSURE	DENSITY	P 0
	FT/SEC)	(0EC)	ш	ILLIBA	LZ.	9 E0
0.0	106	277		212+0	Or (666
00	107	277	0	1206+0	• 1970+03	666
3 0	108	274	50	201+0	S)	0 0
00	106	272	0 0 10	1195+0	5))))
00	m;	271	0	1189+0	5	7 0
500	ស : ស : ស : ស : ស : ស : ស : ស : ស : ស :	269	\$ 6.00 C C V I	1183+03	4 L 4 2 6 6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	ס יכ
000) (C	197	0.00-	11/010		0
	n c	7 6 5	יים ל היים ל היים ל	7 V 4 C	0.191010 0.101010	0 0
) C	696	D 6 C 0 -	3 14 1 4 0		00
0 0	ם כ	202	4 - 1	10.40	, a	0.0
00	701	25.7	1	1149+0	1 60	66
000		0 00 1 (V	1 1 (7) 1 (7) 1	14440	=	
00) C.	257	-63.9	1138+C	12	6
00	,	255		1133+0	ä	*6666-
	4 -	0000 Ture	1 49	1127+0	8	0
) C	,, r.	0 to	4 - C	100+0		666
000	4 -	2000		1116+0		6666
3 (٠.	7 i C	1	711140	-	6666
000	4 -	20.5	# P P P P P P P P P P P P P P P P P P P	110640		.6666-
	4 +	, ii	4 9 (3) 1) (3) (4)		: =	6666
00	40	25.5	-67.2	1 195+0		*6666-
2 0	سو ۾	ានា ប្រហ	1 M 3 C 1 V 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0+060	-	6666
2	* C	253	4.04-	108440	-	666
000	6	1 2 5 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5) o i	.1079+03	-	666
000	-4	258	-60.5	1074+0	17	O.
300		259	*63.6	0+690	*1752+03	6
00.	-	261	-60.7	1063+0	a	6
000	0	264	6.0	1058+0	-	. 6666-
200	10	265	-60.9	1053+0	.1728+03	°6666-
00	105	265	-61.0	.1048+03	,1721+O3	66
00		267	-61.1	1043+C	.1713+O3	* 6666-
00	C	268		1038+0	.1705+03	<u>ر</u> م
ຂຸດດ	O	268		· 1033+03	Ξ,	*6666 -
10¢	0	271	-	1028+0	• 1690+03	- 1:
ם כם	σ,	272	161	* I UZ 3 + U 3	₽:	8 C C C C C C C C C C C C C C C C C C C
000	o lo	213	-	7 10101	7	*0000
	0.0	1 7 7	•	1 0 0	4 4	. ~
000	0 1	212	1,14	1003+0	1652+13	*6666-
300	٠ ٢	271	8 9 1	0.0	7	*6666-
000	٠Î۴۰	696	-61.9	9931+0	16	°6666-
000	٠.	274	-61.0	9883+0	1630+0	666
Sun) vo	27.0	-62.0	9834+0	1622+7	• 6666-
	.9	256	-62.0	9786+0	615+0	° 6666-
000	ഹ	266	-62.1	9739+0	1607+0	0
000	•	265	*62.2	0+1696	1600+	•6666-
700	066	263	-62.2	+ 11 19	593+0	66
900	9	263	-62.3	297+C	585+	9
					-	

(FT) (SS300	17/SEC) 075 075 075 075 082 083 089 089 089 089 089 089 089 089 089 0132 0132 0143 0143	(DEG) 264 264 265 266 266 267 267 267 268 268 268 280 290	(DEG C) -62.4 -62.5 -62.5 -62.7 -62.7 -62.9 -62.9 -63.0 -64.8	(MILLIBARS) • 9503+C2 • 9456+D2 • 9416+D2 • 9364+D2 • 9378+D2 • 9273+D2 • 9277+D2 • 9187+D2 • 9187+D2	(GRAM/W3) • 1571+03 • 1564+03 • 1557+03 • 1549+03 • 1535+03	(PEG C) -99999 -99999 -99999
5000 5100 5100 5100 5100 5100 5100 5100	0.75 0.75 0.75 0.75 0.82 0.83 0.83 0.83 0.83 0.83 0.83 0.83 0.83	'U 'U 'U' 'U 'U' 'U 'U' 'U 'U' 'U 'U' 'U 'U	62.6 62.5 62.5 62.6 62.8 62.8 63.0 64.8 64.8 64.8	ala ala ala ala ala a	. 1571+03 . 1564+03 . 1557+03 . 1549+03 . 1542+03	00000
		264 264 266 266 266 266 267 268 264 264 302 303 303 303	-62.5 -62.5 -62.6 -62.7 -62.9 -63.0 -63.0 -64.8 -67.9 -67.9	9456+0 9410+0 9364+0 9318+0 9273+0 9132+0 9132+0	.1564+03 .1557+03 .1549+03 .1542+03	666
	- N - a a a a a a a a a a a a a a a a a	264 266 266 266 266 266 268 268 268 268 268	62.65 62.65 62.07 62.09 62.09 63.00 64.08 64.08	9410+0 9364+0 9364+0 9273+0 9273+0 9137+0 9093+0	1557+03 1549+03 1542+03 1535+03	66
4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		267 266 266 266 266 268 268 268 268 268 272 280 292 301	-62.6 -62.7 -62.7 -62.7 -62.9 -63.0 -64.8 -67.9	9364+0 93164+0 9273+0 9227+0 9137+0 9093+0	• 1549+03 • 1542+03 • 1535+03	66
	- or	266 266 266 266 266 266 267 267 280 292 301 301	162.7 162.0 162.0 163.0 164.8 164.8 167.9	9318+0 9273+0 9227+0 9182+0 9137+0	• 1542+03 • 1535+03	66
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		266 267 267 269 269 264 264 267 280 292 301 301	162.7 162.9 162.9 163.0 164.8 167.5 167.5	9273+0 9227+0 9182+0 9137+0	.1535+03	
	0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1 1 1 1	267 266 266 269 269 264 264 267 267 267 294 303 303	-62.8 -63.0 -63.0 -63.1 -64.8 -67.5	9227+0 9182+0 9137+0 9093+0	2010CH1	66
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	264 269 269 269 264 264 267 272 272 272 230 302 301	-62.9 -63.0 -63.1 -63.1 -64.8 -67.9 -67.9	9182+0 9137+0 9093+0	CD.07CT.	666
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	266 269 269 264 264 267 272 280 294 302 301 292	-63.0 -63.1 -64.8 -67.5 -67.9	9137+0	.1521+03	O
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	269 269 264 264 264 267 292 302 301 292	-63.0 -63.1 -64.8 -67.5 -67.9	9093+0	.1514+03	6666-
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	269 264 264 264 267 280 290 301 292	-63.01 -64.8 -67.5 -67.9	0.00	.1507+03	6666-
	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	264 264 264 267 280 280 294 301 292	-64.8 -67.5 -67.9 -67.6	?	.1501+03	66
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	264 264 267 280 280 294 302 301	-67.5 -67.9 -67.6	8612+0	• 1440+03	66
	000 4 M C	264 272 230 294 302 301 292 292	-67.9 -67.6	Ü	.1388+03	6666-
	0 0 1 1 1 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1	267 230 294 302 301 292 292	-67.6	7790+0	.1322+03	66
		272 280 294 302 301 292 292		J	.1256+33	66
0 0 0 0 0	W C	280 294 302 301 292 292	-65.8	7047+0	.1184+03	66
W 4 C C		294 302 301 292 292 292	-62.5	6706+0	.1109+03	6666-
		302 301 292 258	-63.2	6384+0	.1059+03	66
500		301 292 258	-63.4	Ö	.1009+03	6666-
1.0		292	-63.2	5786+0	.9601+02	6666-
		8.00	-63.0	5508+0	.9131+02	6666-
15	- 1		-63.8	5243+0	.8725+02	6666-
.0	O	236	4.49-	.4991+02	.8329+D2	666
6	-	236	•	4750+0	.7923+02	6666-
0		244	-63.3	.4522+02	.7567+02	6666-
0	10	247	-62.0	• 4305+02	•7103+02	6666-
20	O	103	-60.5	4101+0	.6718+02	6666-
M	1	109	-58.7	3907+3	•6347+32	6666-
. C	•	129	-58.6	.3723+02	•6045+32	6666-
50		130	#58.8	.3549+62	.5768+02	6666-
.0	•	D60	-56.6	.3383+02	.5442+02	6666-
12	101	081	-55.8	.3226+62	.5171+92	6666-
80	n	083	-56.1	.3076+02	.4937+02	6666-
7900	m	388	-56.5	2933+E	.4716+02	6666-
080300	m	160	-55.8	-2797+02	.4483+02	6666-
8100	m	#6€	0. 55 -	2668+0	Ö	0
200	m	197	-54.0	.2545+02	.4046+02	6666-
8300	N	103	-52.8	2428+0	C	6666-
8400	N	102	-	.2317+02	디	6666-
8500	m	760	Ġ	2213+0	20+444E*	66661
8600	m	194		.2113+02	.3287+92	01
8700	3	σ	3	2018+0	.3124+02	0.0
80	3	0	9	.1928+02	*2959+02	666
8900	l CO	œ		• 1843+G2	.2817+02	666
9000	ഗ	00	•	.1762+02	.2680+32	→ (
9100	ഗ	(O	2	.1684+02	.2547+32	666
9200	٠Ç,	0	-41.6	611+0	.2424+02	6
593000	90	260		+1+	.2316+02	0 0
9400	9	0	-41.7	474+0	•2216+35	***

STS NUMBER 13

TABLE 4. (Continued)

ء ⊦ لد	0 0	NOTICE OF CALL	TEMPERATURE	PRESSURE	DENSITY	9 A
213	77.0	TETO TAIT	נחפה כי	IL LIBA	(GRAM/M3)	ω W
	755	144	5.81.	576+0	.2153+01	66
	623	357	-17.2	+	.2062+01	66
	520	7 C 4 P	0.00	1455	993+	66
	013	2.2.5	ما		.1893+01	*6666=
	ביים ביים	0 10 C	-10.1	134	.1780+01	-6666-
	070	25.5	-7.2	-	69	0
	מיים מיים	3 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	-6.2	1244	,1624+U1	6
	040	000	8.5	1198	.1576+01	° 6666-
	0 F	0 10 00 00 00 00 00 00 00 00 00 00 00 00	-12.2	1152	.1537+01	• 6666-
	2 5			1108	.1471+01	• 6666-
	2 4	247	0	1066	.1404+01	-6666-
The second of th	7 10	076	α (025	.1350+01	•6666-
	U + 10	600	0	9865	.1310+01	·6666-
	04.2	117	211-	9487		•6666-
	0.33	282	4 U	0.014.016	1210+	-6666-
	C27	282	6.01	00+44-0	1158+	*6666-
	025	280	1.61	00+02-0	1103401	•6666-
	027	281	7.01	1 4 4 0	1051+01	666
	030	286	0 · ·	3 1 0 5	4000	-6666-
	032	289	-1.2	-11	0046770	0000-
	033	290	-1.2	~ I	00+400	666
	033	289	-1.2	-10	00.4000	*6666-
	032	288	-2.2	00148649	00+6940	6666-
	027	288	-5.3	ø١٠	00-70-00	666
	621	287	5	00++0+0	1000 m	6666-
	C18	280	7.11-	Ula	7977+00	-6666-
	018	272	Z*TT=	} u	00+6191	•6666-
	021	268	2-11-	1 L	7406+00	.6666-
173000	625	212	7.710	7 4 4 7	7150+00	• 6666-
	030	280	7.61-) L	-6863+00	* 6666-
	037	271 (200 (30 (30 (30 (30 (30 (30 (30 (0 1 C F		• 6556+00	* 6666-
	240	273	7-0-	00+7474	.6277+00	• 6666-
	0.40	200	, c	4567+00	.6063+00	0
	7 + 0	202	-13.7	. 4392+00	.5898+00	• 6666-
	0 4 5		00 199 1	-37	.5737+00	• 6666-
The second secon	720	204	-19.2	.	.5563+00	6666-
	22.0	284	-19.2	00+1682.	.5345+00	• 6666
	025	271	-17.3	• 3 744 + 00	25.09.4	• 6666
	018	257	-13.0	.3599+00	. 482U+UU	- 0000
	013	237	-12.2	*3461+00	00+0294	N (1
	008	206	-13.4	.3328+00	00+00+	0000
	636	161	-16.1	* 3200+00	00+7864	0000
	600	129		.30/6+00	00+900#	. 0
	010	120		.2956+60	າ ຕ	0000
	C11	119	+	. 2841+CO	200	0000-
	C13	125	-12.0	.2733+00		00001
	C16	131	-10.2	*2629+00	ਤ ਾ	-0000
	020	136	ô	.2529+00	* 335 3 + UD 337 € + OD	6666
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		The second secon				0000

TABLE 4. (Continued)

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0 0 0	CORO CO	2 6	1, C	124	-25.2	126.6	-29-7	1 M 1 M 1 M 1 M 1 M 1 M 1 M 1 M 1 M 1 M	6.45-	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2,522	7.94	127.0	1	7-65-	1412	-43.2	M M S	0. 23) M	-46.2	146.2	6.94.	4-14-	-48.2	-49.2	្ត ខេត្ត ខេត្ត	7.76	D • 5 M	10101	N C	-50.3	Z*6ħ-	T•6ħ-	1.64-	-51.2	U C U	=52°5	152.5 154.2	-52°5 -54°2 -55°2 -57°2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	- 52.5 - 55.6 -	- 552 - 554.5 - 554.2 - 554.2 - 559.3 - 60.3	5000 JU # 12		- 5 5 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	- 52.5 - 55.6 -
0.00	NOTICE ON TA	* OE 6.	1.20	154	0.11) (C)	174	661	222	0,41	240	1 C	0.78	26.1	262	, , , , , , , , , , , , , , , , , , ,	440	7 V	266	790	270	274	586	289	300	313	22 M	331	3.36 4.50	24.5	N A M	344	342	337	325	308		265	265 245	265 265 255 251	255 255 251 251	265 285 281 280 280	265 255 250 250 250	265 255 250 250 250 250	265 251 250 250 250 250 250	265 251 251 250 250 255 255 255	265 255 255 250 250 250 255 255 255 255	255 255 255 250 250 255 255 255 255 255
	MINU SPEEU	7.000	7 6 7 0	3 C	7 7 0	ט נר מינים מינים	7.40	0 C	24.0	7 M 7 J 2 C	0 to 0	0.0	1000	* * * C	0.76) a	L 7.2	1.10		ט מי מי	045	9 M C	C33	628	C27	027	027	028	באט מאט	0.50	200	023	020	016	013		TIO	~	613 716	016 020	013 016 020 023	013 016 020 023 023	013 016 020 023 025 027	013 016 020 023 025 027 027	013 016 020 023 025 027 028	013 016 020 023 025 027 030 030	013 016 020 023 027 027 030 030	013 016 020 023 023 027 030 030 028
		<u> </u>	2 5) c	0 0	7 0	2 C) C		2.5	2 0	2 5		2 0	15	, ,) () E) C	2	3 6		12		C		9		Ö (7 0	20	12	C):	5		9	2 5											000000000000

(FT) 2460an	WINE SPEED	WIND DIRECTION	TEMPERATURE	ESSUP	DENSITY	- 1
#	FT/SEC)	(DEG.)	(DEG C)	118	(GRAM/M3)	CDEG C
1:	620	9 1 (0)	72.	2350-0	4073-01	666-
,	ļ 💬	251	ıl e	230-	7897-11	00
3	• •	710	٠ ٢	2120-0	3729-01	. 6666-
3	•	223	, I	2010-01	.3573-01	66
Š	000	190	∙ •	1910-	10-08-6	66
2	-	160	· (7)	810	.3276-01	-6666-
S	-	142	N	1720-	.3138-01	66
S	N	134	-83.7	630	.2998-01	lo.
3	\sim	129		1550	.2858-11	666
S	M	126	S	1476-	.2724-01	666
56	7	125	•	1390	.2589-01	-6666-
S	3	123	-86.8	32	.2468-01	*6666-
3	LO!	123	00	1250	.2354-01	0
5	•	122	α	.1180-01	.2231-01	*6666 -
9	- 9	121	7	1134-	.2143-01	-6666-
3	S	121	6.98-	.1089-01	.2059-01	666
9	S	121	-85.9	.1046-01	10-77-01	.6666-
9	S	121	-85.□	1005-0	.1950-01	6666-
9	S	121	D•#8-	0653-0	.1825-01	66
9	3	121	-83.0	9273-0	.1753-01	6666-
9	3	121	-82.0	908-0	.1684-01	6566-
9	す	121	-81.1	557-C	.1618-01	6666-
30	3	121	-80.1	220-0	.1554-01	6666-
5	3	121	-79.1	897-0	.1493-01	66
2	M	120	-78.1	586-0	.1434-01	6666-
7	M	120	-77.2	287-0	.1378-01	6666-
2	M	120	m76.2	0-000	.1323-01	°6666-
r,	\sim	120	-75.2	.6725-02	.1271-01	6666-
7	N	120	-74.2	460-0	.1221-01	6666-
_	M	et :	_	5540-0	-9740-32	666
8	M I	132	r 11	760-0	.84CD-D2	6666-
30 (m (121	- 1	080-0	7240-02	6
0 0	VIC	108	- 1	2200-0	20-0429*	6666-
ה ה	v	# (C	~ (20-085 G	, (
7 0	VII	670	20 C	0-0/67	70=0+9+•	6666
) O	າເ	997	ρo		20100+ 60104+	00001
0 -	ule	203	6.70-		20-0556	
3 27	4 C	3.05	1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	- 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20-05-05-05-05-05-05-05-05-05-05-05-05-05	0 4
-	i N	279	-83.9	126-0	.2030-02	6666-
=	3	271	, CC	0-0946	1730-92	66
2	(0)	269	-83.9	8030-0	.1460-02	0
91	•	569	-82.6	6830-G	1230-	• 6666-
51	S.	269	81.	810-0	1030-0	66
2	IO!	269	00	0-046	710-5	666
S	-	268	78.	200-0	7330-0	0
8	m	266		580-0	180-0	•6666-
2	035	267	73	.3070-03	.5180-03	6666-
7	mi	266	-69.7	630-0	350-0	6666-

TABLE 4. (Concluded)

THE PROPORTION OF A PART	א - ארני ארני					
ALTITUDE	WIND SPEED	WIND DIPECTION	TF MPER ATURE	PRESSURE	DENSITY	DEW POINT
(FT)	(FT/SEC)	(DEG)	(DEG C)	(MILLIBARS)	(GRAM/M3)	(DEG C)
340000	0.45	263	-61.8	.1940-03	. 3060-03	•6666-
343000	8 40	261	-57.8	.1660-03	.2570-03	* 6666-
346000	049	264	525.5	.1440-03	.2170-03	· 6666-
349300	C50	262	7.54-	.1270-03	.1850-03	• 6666-
352300	049	258	-39.0	.1110-03	.1570-03	•6666 -
355300	247	254	*32°3	40-0176	.134C-D3	-6666-
358300	C#3	742	-25.5	. P570-04	.1140-03	-6666 -
361000	C33	250	13.7	*7520~04	+G-0016*	-6666 -
364000	534	244	8.6-	.6790-04	.843E=34	.6666
367300	035	236	٥.1	.6120-04	.7330-04	*6666**
370000	036	226	6°2	.5510-04	.6370-04	*6666 *
373300	039	214	16.8	40-096h°	*554D=04	*6666 **
376030	770	201	25.8	, 4 460 mD4	.4820-04	*6666*
379200	627	206	35,3	* 4 O 4 O * O *	. 4220-04	•6666 -
382300	D29	203	3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.3700-64	.373C-04	°6666-
385000	032	199	56.3	#D-0622°	*3300-04	* 6666-
388000	D34	197	67.2	.3120-04	,2930-04	* 6666-
391000	037	194	78.4	,288D-D4	,2610-04	*6666*
394000	041	192	89.9	,2670-04	•2340=04	°6666-
397300	##O	190	101.5	*2480-C4	.2100~04	*6666-
430300	8 3 C	189	113,3	.2300-04	.189C-04	* 6666 -

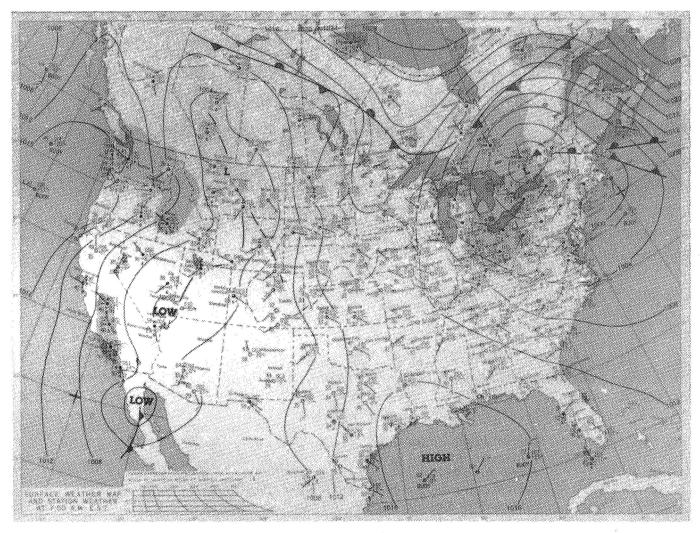
SELECTED ATMOSPHERIC OBSERVATIONS FOR THE FLIGHT TESTS OF THE SPACE SHUTTLE VEHICLES TABLE 5.

	,	Count Down and Launch Comments of Meteorological Significance			Wind directional change observed at Pad just prior to L+0. Onset of sea breeze.					17 min countdown delay due to adverse weather conditions.			×
tions	ft	Dir. (deg)	250	286	250	329	336	277	278	349	252	288	289
Inflight Conditions	Max. Wind Below 60,000 ft	Speed (ft/sec)	86	158	119	37	146	155	92	30	117	143	176
Inflig	N Belo	Alt. (ft)	44,300	36,300	45,000	47,900	40,600	46,100	45,900	45,100	47,100	38,200	37,700
	Wind ^b	Dir. (deg)	125 120	345 355	50e 145e	133g 141g	06	63 55	10 ^e 350 ^e	269	183 190	0 NA	320 275
su		Speed (ft/sec)	11.8 15.2	27.0 27.0	7.0e 8.0e	5.8g 4.9g	22.0 35.0	12.7 16.4	5.9^{e} 10.3^{e}	8.8 14.0	$\frac{19.1}{32.0}$	0.0 NA	21.5 18.6
servatic	Thermodynamic ^a	Rel. Hum. (%)	83	61	7.1	7.0	89	55	08	26	83	75	56
Surface Observations		Temp.	21	23	24	29	22	23	25	24	24	17	16
		Press. N/cm ²	10.234 ^d	10.166	10.160	10.200	10.227	10.183	10.146	10.111	10.153	10.173	10.149
		Launch Pad	39A	39A	39A	39A	39A	39A	39A	39A	39A	39A	39A
	: ::	Time (EST) Nearest Minute	0040	1010	1100	1100^{f}	0719	1330	0733^{f}	$0232^{ m f}$	1100	0800	0858
	Vehicle Data	Launch Date	4/12/81	11/12/81	3/22/82	6/27/82	11/11/82	4/4/83	6/18/83	8/30/83	11/28/83	2/3/84	4/6/84
in the second se		Vehicle No.	STS-1 Columbia	STS-2 Columbia	STS-3 Columbia	STS-4 Columbia	STS-5 Columbia	STS-6 Challenger	STS-7 Challenger	STS-8 Challenger	STS-9 (SL-1) Columbia	STS-11 (41-B) Challenger	STS-13 (41-C) Challenger
		Seq.	,-	83	ო	4	ro	6	2	∞	6	10	Ħ

က် Pad 39A thermodynamic measurements taken at approximately 1.2 m (4 ft) above natural grade at camera site No. 1 min average prior to L+0 of 60 ft PLP (listed first) and 275 ft FSS winds measured above natural grade. Pressure measurement applicable to 21 ft above MSL unless otherwise indicated. Pressure measurement applicable to 14 ft above MSL.

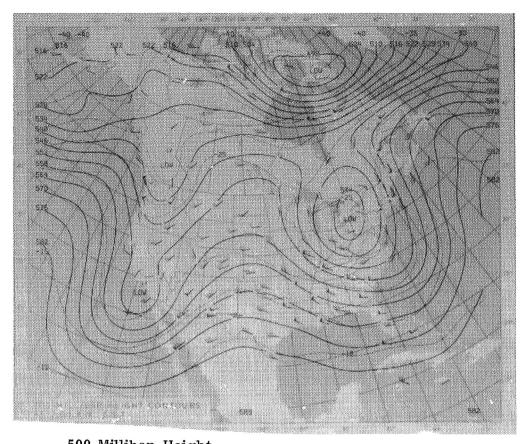
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¹⁰ sec average prior to L+0. Eastern Daylight Time. 30 sec average prior to L+0.



Surface Synoptic Map at 1200 UT April 6, 1984 — Isobaric, Frontal, and Precipitation Patterns are Shown in Standard Symbolic Form.

Figure 1. Surface synoptic chart 1 hr 58 min prior to launch of STS-13.



500 Millibar Height
Contours at 1200 UT
April 6, 1984.
Continuous Lines Indicate Height Contours In Feet
Above Sea Level. Dashed Lines are Isotherms In
Degrees Centigrade. Arrows Show Wind Direction
and Speed at the 500 MB Level.

Figure 2. 500 mb map 1 hr 58 min prior to launch of STS-13.

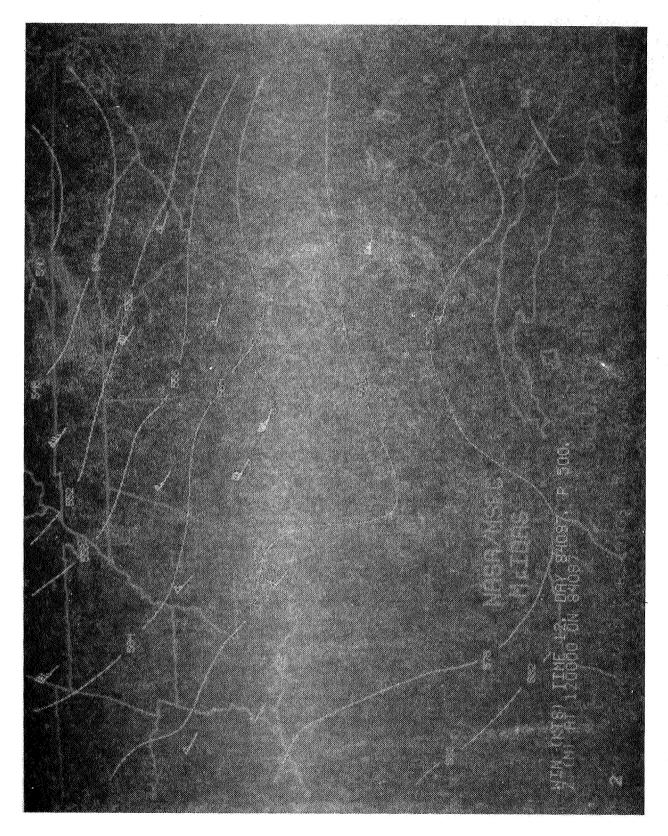


Figure 3. GOES-5 visible imagery of cloud cover 2 min after launch of STS-13 (1400 UT, April 6, 1984). 500-mb contours and wind barbs are also included for 1200 UT.

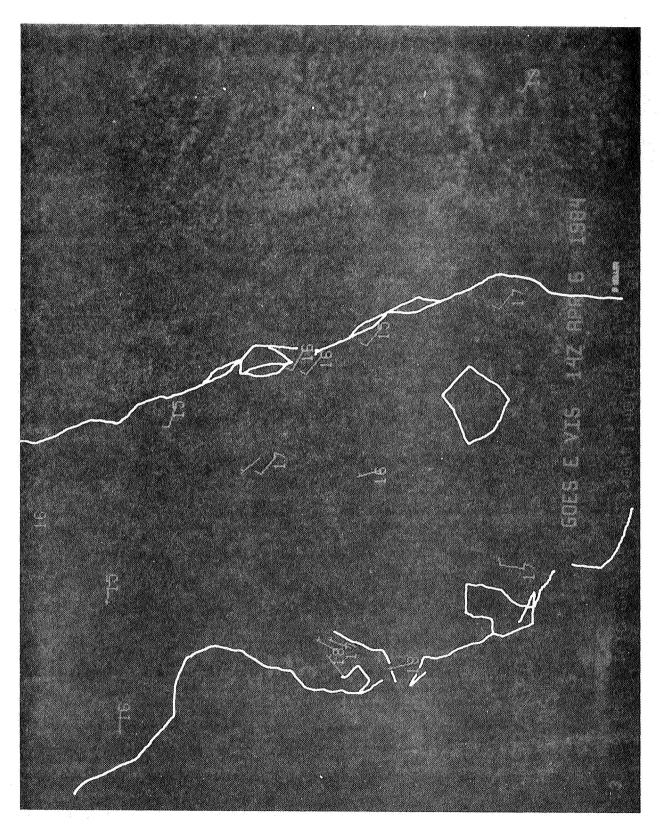


Figure 4. Enlarged view of GOES-5 visible imagery of cloud cover taken 2 min after launch of STS-13 (1400 UT, April 6, 1984). Surface temperatures and wind barbs for 1400 UT are also included.

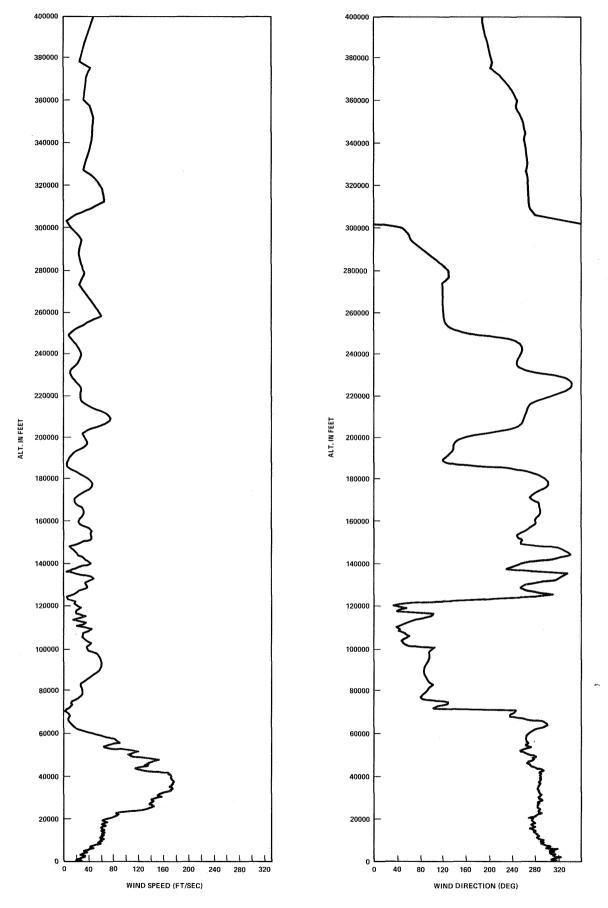


Figure 5. Scalar wind speed and direction at launch time of STS-13.

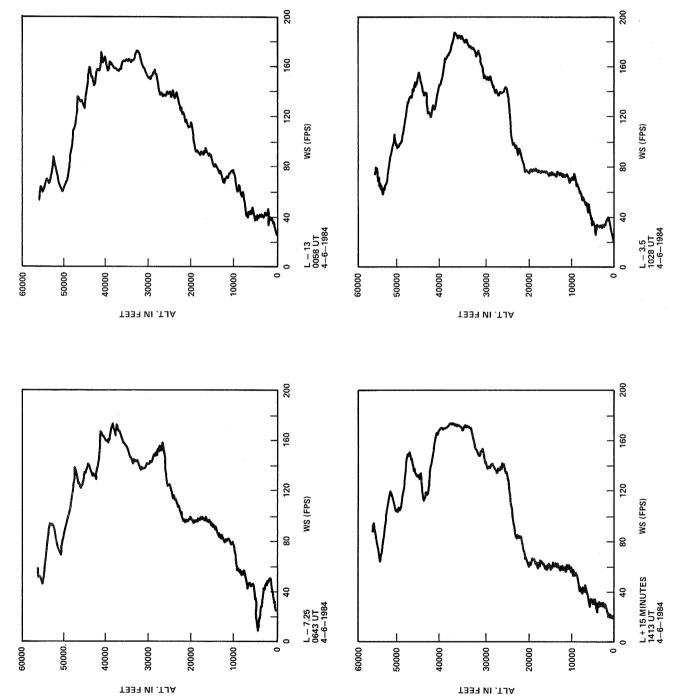
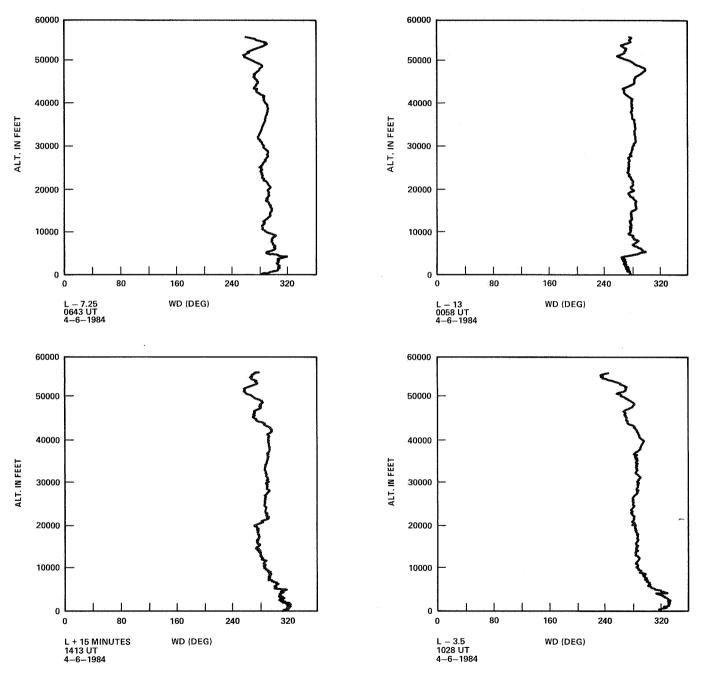
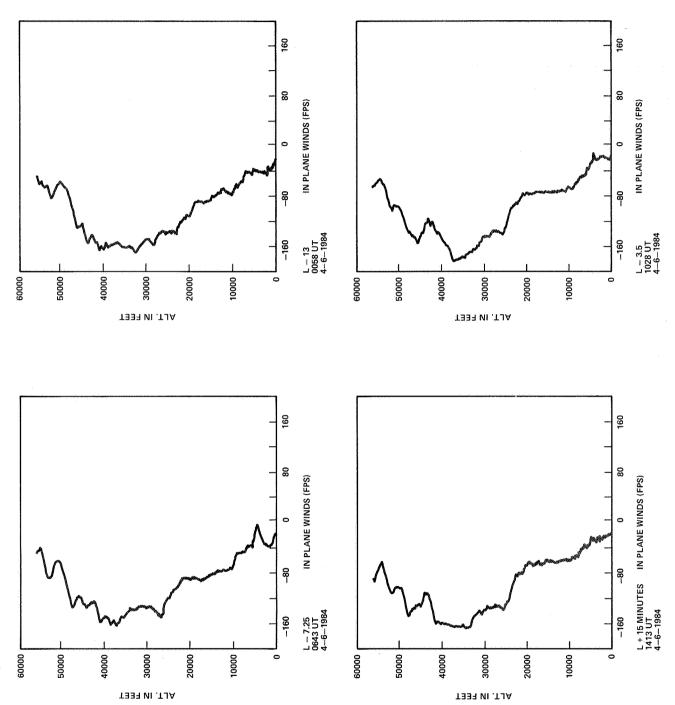


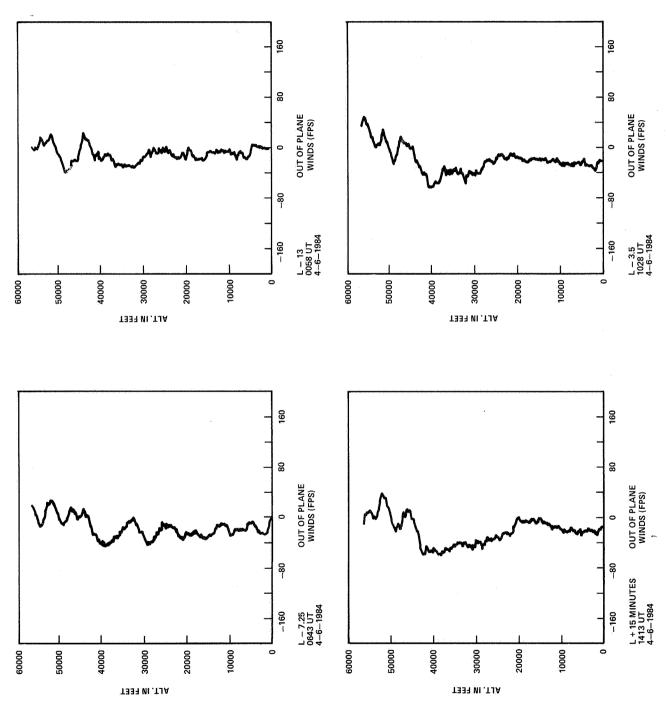
Figure 6. STS-13 prelaunch/launch Jimsphere-measured wind speeds (FPS).



STS-13 prelaunch/launch Jimsphere-measured wind directions (degrees). Figure 7.



STS-13 prelaunch/launch Jimsphere-measured in-plane component winds (FPS). Flight azimuth = 91 degrees. Figure 8.



STS-13 prelaunch/launch Jimsphere-measured out-of-plane components winds (FPS). Flight azimuth = 91 degrees. Figure 9.

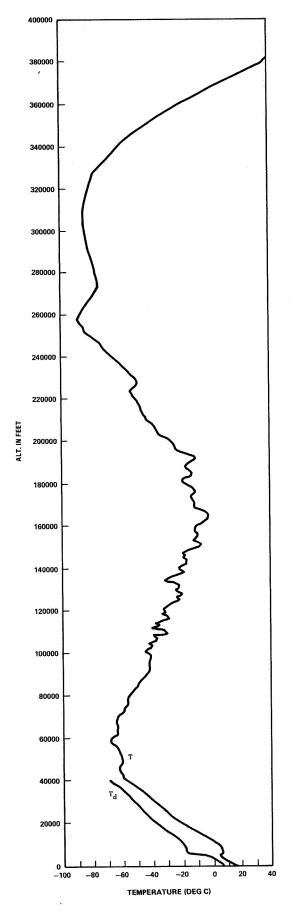


Figure 10. STS-13 temperature profiles versus altitude for launch (ascent).

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APPROVAL

ATMOSPHERIC ENVIRONMENT FOR SPACE SHUTTLE (STS-13) LAUNCH

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The information in this report has been reviewed for technical content. Review of any information concerning Department of Defense or nuclear energy activities or programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

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